International Journal of ELECTROCHEMICAL SCIENCE www.electrochemsci.org

A Comparative Study on the Electrochemical Behaviour of Aluminium and 8090 Al- Li-Cu-Mg Alloy in Acid Rain Solution

Zora Pilić^{*} and Ivana Martinović

Department of Chemistry, Faculty of Science and Education, University of Mostar, Mostar, Bosnia and Herzegovina *E-mail: zora.pilic1@gmail.com

Received: 10 February 2017 / Accepted: 18 March 2017 / Published: 12 April 2017

The growth mechanism and properties of the oxide films on aluminium and 8090 Al-Li-Cu-Mg alloy were studied in simulated acid rain (pH 4.5) by electrochemical techniques, cyclic voltammetry and electrochemical impedance spectroscopy. The potentiodynamic formation of anodic oxide film on aluminium and 8090 Al-Li-Cu-Mg alloy surfaces were described in terms of high field model. This is justified by the obtained values of kinetic parameters: the electric field strength ($\sim 10^6$ V cm⁻¹), ionic conductivity through the film ($\sim 10^{-12}$ S cm⁻¹ and 10^{-13} S cm⁻¹) and half jump distance (~ 0.150 nm). The impedance data shows that protective passive oxide film on aluminium and Al-Li-Cu-Mg alloy can be formed spontaneously at the open circuit potential in the studied solution with a high resistance (119 k Ω cm² for Al and 144 k Ω cm² for Al-Li-Cu-Mg alloy has better protective properties than pure aluminium. The concentration of the metallic ions released into solution from aluminium and Al-Li-Cu-Mg alloy and measured by atomic absorption spectroscopy was in accordance with the results obtained from the electrochemical techniques.

Keywords: Aluminium, 8090 Al-Li-Cu-Mg alloy, Anodic film, Simulated acid rain, Cyclic voltammetry, Electrochemical impedance spectroscopy, Atomic absorption spectrometry.

1. INTRODUCTION

Aluminium and its alloys are of great technological significance and widely applied in a variety of fields due to their strong resistance to corrosion. The main reason for the corrosion resistance of aluminium is the formation of a thin and protective oxide film which separates the bare metal from the corrosive environment. The oxide film on aluminium is formed spontaneously in contact with moist air or aqueous solution, but can also be formed by anodic polarization, which can increase film thickness

and resistance [1–9]. The stability of the oxide film on aluminium depends on temperature, chemical composition and pH of the electrolyte, while the thickness of the anodic film is determined by the applied anodizing potential [1].

A passive oxide film forms naturally on the aluminium surface under usual atmospheric conditions and it is stable in environments with pH between 4 and 9. However, in polluted atmospheric conditions (even in pH range in which the oxide film is stable), the protective surface film can be destroyed and corrosive attack takes place due the presence of aggressive ions [10, 11]. Aggressive anions degrade the oxide and cause film breakdown and pitting corrosion.

Acid rain corrosion has become an increasing concern due to increasing air pollution as a result of industrialization and the burning of fossils fuels containing gaseous acid oxides. These oxides dissolve in the rain forming the acid rain. The acid rain conditions lead to the deterioration of water quality, human health as well as metals subjected to polluted environments. The investigation of the corrosion mechanism of metals in different harsh environments enables their longer use and in the same time producing less waste and using less energy.

Gerengi et al. [11, 12] investigated the corrosion behaviour of aluminium 6060 and 6082 by scanning electron microscopy, atomic force microscopy, potentiodynamic polarization and dynamic electrochemical impedance spectroscopy in simulated acid rain, as well in pure water. Their measurements reveal that the pH of the studied environment is very effective on electrochemical corrosion process and that the protection film formed in the absence of acid rain has great importance against corrosion. They showed that the AA6060 and AA6082 have similar corrosion behaviours in pure and acid rain environments, but the AA6060 alloy was more resistant to corrosion in an acid rain environment than the AA6082 alloy.

Aluminium alloys containing lithium are potential materials for the aerospace applications due to their increased specific strength and elastic modulus and lowered density compared to the conventional used aluminium 2xxx and 7xxx series [13–16] alloys.

The electrochemical behaviour of 8090 Al- Li-Cu-Mg alloy was subject of several papers, but there are many disagreements about the corrosion behaviour of this alloy. Ricker and Duquette [17] found an increased corrosion susceptibility of an Al–4.2 Mg–2.1 Li alloy compared with the 7050 (Al–6.5Zn-2.4Mg-2.2Cu) alloy. De Jong and Martens [18] found that the pitting potential of Al– Cu–Mg (–Li) alloys became slightly more negative with lithium additions. In this investigation the kinetics of growth and electrochemical properties of the oxide films on the aluminium and 8090 Al- Li-Cu-Mg alloy in simulated acid rain, *pH* 4.5 was studied by using the electrochemical techniques of cyclic voltammetry (CV) and electrochemical impedance spectroscopy (EIS). The concentration of Al ions released during the oxidation process was performed using atomic absorption spectrometry (AAS).

2. EXPERIMENTAL PROCEDURE

Aluminium (99.99 %) and 8090 Al- Li-Cu-Mg alloy, with a composition (wt.%) of 2.50 Li, 1.40 Cu, 1.10 Mg, 0.08 Zr and the remainder Al were used as working electrodes. The surface areas of the Al and 8090 Al- Li-Cu-Mg alloy samples, exposed to the electrolyte, were 0.636 cm² and 0.502

cm², respectively. The electrodes were mechanically abraded by 1200 grade emery paper, degreased with ethanol in an ultrasonic bath and rinsed with ultra pure water (18.2 M Ω cm, produced by Millipore Simplicity UV Water Purification System). Prior to each measurement electrodes was polarized at -1.60 V vs. Ag | AgCl | 3 M KCl electrode for 120 seconds to remove air-formed oxide from the surface.

The electrochemical measurements were performed at room temperature in a standard three electrode cell. The counter electrode was a platinum electrode and the reference electrode, to which all potentials in the paper are referred, was an Ag | AgCl | 3 M KCl.

The electrolyte was a simulated acid rain solution. Chemical composition of the simulated acid rain [19] is given in Table 1. The pH value of solution was 4.5 and electrical conductivity 1.306 mS cm⁻¹. pH value was adjusted by the addition of the appropriate amount of 0.5 mol L^{-1} H₂SO₄. All chemicals were of p.a. purity and obtained from Sigma Aldrich.

Table 1. Chemical composition of the simulated acid rain solution (g L^{-1}).

NH ₄ NO ₃	$MgSO_4 \cdot 7H_2O$	Na_2SO_4	KHCO ₃	$CaCl_2 \cdot 2H_2O$
0.13	0.31	0.25	0.13	0.31

Electrochemical techniques, cyclic voltammetry and electrochemical impedance spectroscopy were performed with an Autolab PGSTAT320N controlled by a personal computer using Nova 1.5 software. CV measurements were carried out in the potential range between -1.60 V and -0.20 V, with scan rates from 10 to 100 mV s⁻¹.

EIS measurements were carried out in the frequency range between 10 kHz and 5 mHz with the *ac* amplitude ± 10 mV at constant potential. EIS measurements were performed at the open circuit potential, E_{OCP} (-0.485 V) and on E = -0.850 V for both, aluminium and 8090 Al- Li-Cu-Mg alloy. Prior to each measurement the electrodes were stabilized for 30 min at the selected potentials. This procedure gave good reproducibility of results.

The concentrations of the Al ions released into simulated acid rain solution after 60 minutes of specimens' immersion at open circuit potentials were obtained by atomic absorption spectrometry. Since the EIS measurements lasted approx. 60 minutes, the concentration of released ions was determined after this period of time.

3. RESULTS AND DISCUSSION

3.1. Cyclic voltammetry

The cyclic voltamograms of the aluminium recorded in a simulated acid rain solution with increasing scan rates from 10 to 100 mV s⁻¹ are presented in Fig. 1a. During the anodic sweep the current profile shows two anodic peaks that are shifted towards higher current densities with increasing

scan rate. The first oxidation peak, A_1 , at around -1.40 V, is related to the initial phase of oxide growth [1]. In this phase mobile Al ions accumulate at the interface metal/solution but because of small amount of ions electric field strength is insufficient to move them. The second anodic peak A_2 , at around -0.90V can be ascribed to the formation of a Al(III) oxide. At potentials more positive than -0.90 V, current profile reaches a steady-state value (j_{pl}) that remains constant up to -0.30 V. This is a passive region where oxide film is thickening with increasing anodic potential [1, 7, 20]. Similar potentiodynamic E-j profiles were also obtained for Al-Li-Cu-Mg alloy in the same solution (Fig. 1b.).

During the cathodic sweep there is no presence of cathodic reduction of alumina film formed during the anodic sweep. Cyclic voltammograms obtained indicate that the formation of oxide films on the surfaces of Al and Al-Li-Cu-Mg alloy is a typical irreversible process [1, 7, 20]. At low scan rates ($\leq 10 \text{ mV s}^{-1}$) the Al-Li-Cu-Mg alloy undergoes pitting corrosion at potential higher than -0.5 V. Aluminium–lithium alloys are susceptible to pitting corrosion [21].



Figure 1. The cyclic voltammograms of (a) Al and (b) 8090 Al-Li-Cu-Mg alloy recorded in simulated acid rain with increasing scan rates.



Figure 2. (a) Values of the peak current densities (j_p) as a function of scan rate, and (b) values of the logarithm of peak current densities $(\log j_p)$ as a function of logarithm of scan rate $(\log v)$ for peak A₂. The peak current density values were obtained from Fig. 1.

Analysis of the influence of scan rate, v on the current density, j_p of anodic peak A_2 showed that current density of anodic peak A_2 increases linearly with the scan rate and potential of peak A_2 shifts to more positive values. Changes in scan rate had no influence on the value of cathodic current density i.e. the cathodic current density was independent of the scan rate [1].

Linear dependences of peak current densities, j_p on the scan rate, v(Fig. 2a) and of log j_p on the log v with the slope ≈ 1 (Fig. 2b) are obtained for peak A₂ for both materials, Al and Al-Li-Cu-Mg alloy. The obtained linear relationship indicates kinetic control of the oxidation process of Al in Al₂O₃, with charge transfer being the slow step of the reaction [20].

3.2. Formation and growth of the anodic film

The steady state values of current density, in the potential range from -0.8 to -0.3 V indicate steady state film growth in the passive region. Obtained linear dependence between $\log j_{pl}$ and values of (ν/j_{pl}) (Fig. 3) indicates that growth of the oxide film on the Al and Al-Li-Cu-Mg alloy takes place due to the ionic conductivity under the high electric field within the oxide film described by [22–25]:

 $j_{\rm pl} = A \exp(B\varepsilon) \tag{1}$

where j_{pl} is the ionic current density for oxide growth, ε is the electric field within the oxide, and *A* and *B* are temperature-dependent parameters of the oxide. For the potentiodynamic oxide growth, provided that the potential drop at the interfaces is negligible and in the absence of space charge effects, the following expression for the steady-state current density (j_{pl}) is valid [23, 25]:

$$\log j_{\rm pl} = \log A + (z F B / 2.3 V_{\rm m}) (v / j_{\rm pl})$$
(2)

where $V_{\rm m}$ is the molar volume of the growing phase and ν is the scan rate.

Under the assumption that on both, Al and Al-Li-Cu-Mg alloy the oxide layer is mostly composed of Al₂O₃ ($M = 102 \text{ g mol}^{-1}$ and $\rho = 3.2 \text{ g cm}^{-3}$; $V_{\rm m} = 31.88 \text{ cm}^3 \text{ mol}^{-1}$) [1, 26, 27], the kinetic parameters *A* and *B* were determined from intercept and slope of the linear dependence log $j_{\rm pl}$ vs. (ν / $j_{\rm pl}$) and shown in Table 2. Obtained values are in an agreement with reported values [1]. The product of *A* and *B* represents the ionic conductivity of the oxide layer during growth. Values are also shown in Tab. 2.

The values of half jump distance for aluminium ions, *a* were calculated according to the theory of high field ion transport [1, 28, 29]:

$$B = \frac{a^* zF}{RT} \tag{3}$$

where z is the valency of the moving ion, F is the Faraday constant, R is the gas constant and T is the temperature and presented in Tab. 2. The values of electric field strength were calculated according to the equation (1) using values of j_{pl} (Fig. 1, Tab. 2) and also presented in Tab. 2. The obtained values of the electric field strength (10^6 V cm⁻¹) and kinetic parameters confirm that the growth of oxide film on the Al and Al-Li-Cu-Mg alloy in a simulated acid rain solution takes place due to the ionic conductivity under the influence of the high electric field [3, 7, 20, 30-33]. Anodic film growth takes place due to the migration of Al³⁺ and O²⁻ ions through the film under the high electric field [1, 20].



Figure 3. The dependence of $\log j_{pl}$ vs. v/j_{pl} for the anodic growth of Al₂O₃ on the Al and Al-Li-Cu-Mg alloy in simulated acid rain solution.

Table 2. The kinetic parameters for the oxide film growth on the Al and 8090 Al-Li-Cu-Mg alloy in simulated acid rain solution.

material	$j_{\rm pl}$ / mA cm ⁻²	$A / A \text{ cm}^{-2}$	$B / \mathrm{cm} \mathrm{V}^{-1}$	$AB / S cm^{-1}$	ε / V cm ⁻¹	<i>a</i> * / nm
Al	0.032	8.39×10 ⁻⁷	1.765×10^{-6}	1.48×10^{-12}	2.06×10^{6}	0.151
8090 Al-Li- Cu-Mg	0.030	1.38×10^{-7}	1.84×10^{-6}	2.54×10^{-13}	2.94×10^{6}	0.157

The total charge used for film formation, Q_A has been determined by integration of the area under the curve in the obtained anodic part of cyclic voltammograms from Fig. 1 and shown in Table 3. Under assumption that the surface layer on the Al and Al-Li-Cu-Mg alloy is mostly composed of Al₂O₃ oxide [1, 26, 27], its thickness, *d* was calculated from the determined charge, Q_A :

$$d = \left(\frac{M}{\rho z F}\right) \frac{Q_{\rm A}}{\sigma} \tag{5}$$

where *M* is the molar mass of Al₂O₃, ρ is density of Al₂O₃, *z* is the number of electrons, *F* is the Faraday constant and σ is the roughness factor of the surface (σ = 2). The calculated thickness values are shown in Table 3. The calculated thickness value is in good agreement with the literature [1, 30].

Table 3. Anodic charges and thickness of the oxide film on the Al and Al-Li-Cu-Mg alloy in acid rain solution.

material	$Q_{\rm A}$ / mC cm ⁻²	<i>d</i> / nm
Al	8.067	2.21
8090 Al-Li-Cu-Mg alloy	6.193	1.70

Comparison of electrochemical behaviour of Al and Al-Li-Cu-Mg alloy recorded by CV reveals that the oxide film on Al-Li-Cu-Mg alloy shows better properties than those on pure Al. Under same experimental condition currents densities for Al are higher than for Al-Li-Cu-Mg alloy and the width of the passive range is broader for Al-Li-Cu-Mg alloy (Fig. 4). Lower value of film thickness for Al-Li-Cu-Mg alloy (Table 3) also indicates better protective properties. However, at lower scan rates the Al-Li-Cu-Mg alloy undergoes pitting corrosion (Fig 1).



Figure 4. The cyclic voltammograms of the aluminium and 8090 Al-Li-Cu-Mg alloy recorded in simulated acid rain solution. Scan rate, $v = 50 \text{ mV s}^{-1}$.

3.3. Electrochemical impedance spectroscopy

Figure 5 shows the variation of E_{OCP} of Al and Al–Li-Cu-Mg samples with time in the simulated acid rain solution. As can be seen, the Al–Li-Cu-Mg alloy reaches a stable value of $E_{\text{OCP}} \approx -0.485$ V, after 20 min., while pure Al achieves a stable value of $E_{\text{OCP}} \approx -0.485$ V after 1 h.

In order to determine the characteristics and electrical properties of the oxide layer, impedance measurements were performed at open circuit potential and during the anodic polarization, E = -0.850 V.

The electrochemical properties of the oxide film formed on the Al and Al-Li-Cu-Mg alloy in simulated acid rain at the open circuit potential, $E_{OCP} = -0.485$ V were investigated using EIS. The usual criteria for the selection of the best-fit electric equivalent circuits (EEC) are minimum number of circuit elements employed, the χ^2 error suitably low ($\chi^2 \le 10^4$), and the errors associated with each element up to 5 %.



Figure 5. Open circuit potential, E_{OCP} vs. time for Al and Al-Li-Cu-Mg alloy in the simulated acid rain solution.

The impedance spectra for the Al and the Al-Li-Cu-Mg alloy obtained at their open circuit potentials (-0.485 V) are presented in Fig. 6 in the form of Nyquist plots. At this potential, the barrier oxide impedance dominates the total impedance and only one time constant can be observed on Nyquist plots. The responses of the systems were semicircles which is associated with the thickness and dielectric properties of oxide film. The ohmic resistance (R_{Ω}) , visible in the high-frequency region, was 50 Ω cm². The impedance data obtained were analyzed in terms of EEC shown in the detail of Fig. 6. It consists of a *CPE* in the parallel to the resistor *R*. For fitting the spectra a constant phase element (CPE) was used instead of an ideal capacitance element to compensate surface heterogeneities [34, 35]. Its impedance may be defined: $Z_{CPE}(\omega) = [Q(j\omega)^n]^{-1}$, where Q is a constant, ω is the angular frequency and *n* is the *CPE* power with values between 0.5 and 1 [36]. When n = 1, the *CPE* describes an ideal capacitor with Q equal to the capacitance (C). For 0.5 < n < 1, the CPE describes a distribution of dielectric relaxation times in frequency space, and when n = 0.5 the CPE represents a Warburg impedance [37]. The oxide film on Al and Al-Li-Cu-Mg alloy is considered to be the parallel circuit of a resistor due to ionic conduction and a capacitance due to the dielectric properties of the oxide [1]. For the both electrodes, the value of n_1 points that the constant phase element Q_1 is essentially a double layer capacitance, C_{dl} . The charge transfer resistance corresponds to R_1 . Its numerical value indicates the high stability of aluminium and Al-Li-Cu-Mg alloy in the acid rain solution. From the analysis of the impedance data, the resistance and capacitance of the oxide film associated with the high frequency capacitive loop were obtained and presented in Table 4.



Figure 6. Nyquist plot representation of EIS data of the Al and Al-Li-Cu-Mg alloy passivated at the open circuit potential, -0.485 V. Inset: the electrical equivalent circuit used to fit the EIS data.

Table 4. The numerical values of impedance parameters for Al and Al-Li-Cu-Mg alloy in simulated acid rain at $E_{\text{OCP}} = -0.485$ V.

material	$Q_1 imes 10^6$ / $\Omega^{-1} \mathrm{s^n} \mathrm{cm^{-2}}$	<i>n</i> ₁	<i>R /</i> kΩ cm ²
Al	11.52	0.875	119.95
8090 Al-Li-Cu-Mg	6.108	0.955	144.65

The total impedance for impedance spectra recorded at open circuit potential is given by:

$$Z_{\text{tot}} = R_{\Omega} + \frac{\kappa}{RQ(j\omega)^n + 1} \tag{6}$$

The values of R_1 obtained were very high, indicating that the oxide films formed spontaneously at the open circuit potential are very resistive and relatively compact.

Comparing the obtained data (Table 4), it can been seen that aluminium and 8090 Al-Li-Cu-Mg alloy show similar corrosion behaviour in simulated acid rain solution at open circuit potential although the resistance of aluminium is somewhat reduced and capacitance increased in the comparison to the 8090 Al-Li-Cu-Mg alloy.

Impedance spectra obtained at -0.850 V on aluminium and 8090 Al-Li-Cu-Mg alloy are presented in Figure 7 in the form of a Nyquist plots. From the Nyquist plots it is obvious that two time constant can be identified. The impedance data obtained were analyzed in terms of EEC shown in the detail of Fig. 7. The impedance spectra for aluminium may be described by $R_{\Omega}(R_1Q_1)(R_2Q_2)$ equivalent circuit model and for Al-Li-Cu-Mg alloy by $R_{\Omega}(R_1Q_1)(R_2Q_2)$. Q_1 describes the properties of the barrier oxide layer and R_1 the resistance to ion migration through the barrier oxide layer. The low frequency time constant can be related to the properties of the barrier oxide layer/solution interface. R_2 may describe the charge transfer resistance across the interface [38].



Figure 7. Nyquist plot representation of EIS data of the Al and Al-Li-Cu-Mg alloy passivated at the E = -0.850 V. Inset: the electrical equivalent circuits used to fit the EIS data.

Table 5. The numerical values of impedance parameters for Al and Al-Li-Cu-Mg alloy in simulated acid rain at E = -0.850 V.

material	$Q_1 \times 10^6 / \Omega^{-1} \mathrm{s}^{\mathrm{n}} \mathrm{cm}^{-2}$	<i>n</i> ₁	$R_{1}/k\Omega \text{ cm}^{2}$	$Q_2 \times 10^6 / \Omega^{-1} s^n cm^{-2}$	<i>n</i> ₂	$R_2/k\Omega \text{ cm}^2$
Al	16.121	0.946	23.723	86.522	0.774	38.421
8090 Al-Li- Cu-Mg	8.125	0.973	50.777	57.841	0.802	37.723

It can be seen from Table 5 that the 8090 Al-Li-Cu-Mg alloy has higher resistance values and more compact barrier layer than pure aluminium in simulated acid rain solution at E = -0.850 V.

The total impedance Z for the investigated system at E = -0.850 V is given by:

$$Z_{\text{tot}} = R_{\Omega} + \frac{R_1}{R_1 Q_1 (j\omega)^{n_1} + 1} + \frac{R_2}{R_2 Q_2 (j\omega)^{n_2} + 1}$$
(7)

and for Al-Li-Cu-Mg alloy at same potential is given by:

$$Z_{\text{tot}} = R_{\Omega} + \left(Q_1 (j\omega)^{n_1} + \left(R_1 + \frac{R_2}{R_2 Q_2 (j\omega)^{n_2} + 1} \right)^{-1} \right)^{-1}$$
(8)

3.4. Atomic absorption spectrometry

The results obtained in the static immersion test are listed in Table 6. As can be seen from Table 6, a slightly higher quantity of Al was released from the pure aluminium than from the Al-Li-Cu-Mg alloy. These results are in good agreement with the corresponding resistances obtained by electrochemical techniques.

Table 6. The quantities of Al ions dissolved during 1 hour-immersion of aluminium and 8090 Al-Li-Cu-Mg specimens in simulated acid rain at open circuit potential.

material	γ (Al) / μ g dm ⁻³ cm ⁻²
Al	0.126
8090 Al – Li-Cu-Mg	0.120

From the results of AAS it is obvious that corrosion of aluminium and Al-Li-Cu-Mg alloy under acid rain conditions increases the concentration of metals in the environment.

4. CONCLUSION

Cyclic voltammetry and electrochemical impedance spectroscopy were used to study passivation and corrosion behaviours of the Al and Al-Li-Cu-Mg alloy in a simulated acid rain solution with a pH of 4.5. The growth of the anodic oxide film on the Al and Al-Li-Cu-Mg alloy, under potentiodynamic conditions, occurs under a high -field migration mechanism. Values of electric field strength, parameters *A* and *B* characterising the anodic growth, ionic conductivity through the film and half jump distance were determined.

Cyclic voltammetry revealed that Al-Li-Cu-Mg alloy shows better electrochemical properties than pure Al. Thickness of oxide films obtained by analyzing the anodic current curves show that film with better protection properties forms on Al-Li-Cu-Mg alloy (1.70 nm) than on pure Al (2.20 nm).

At the open circuit potential, both pure metal and alloy underwent passivation, indicating that the oxide films formed spontaneously at the open circuit potential are very resistant (144 k Ω cm² for Al-Li-Cu-Mg alloy and 119 k Ω cm² for Al). In case of 8090 Al-Li-Cu-Mg alloy obtained charge transfer resistance value is higher and double layer capacitance is reduced in comparison to pure aluminium.

From the results of AAS it is obvious that corrosion of aluminium and Al-Li-Cu-Mg alloy under acid rain conditions increases the concentration of metals in the environment.

References

- 1. D. Hasenay and M. Šeruga, J. Appl. Electrochem., 37 (2007) 1001.
- 2. G. E. Thompson, *Thin Solid Films*, 297 (1997) 192.
- 3. M. M. Lohrengel, Mater. Sci. Eng., R11 (1993) 243.
- 4. A. Despić and V.P. Parkhutik in: J. O. Bockris, R. E. White and B. E. Conway (Eds) Modern aspects of electrochemistry, vol 20, Plenum Press, (1989) New York, USA.
- 5. J. Bessone, C. Mayer, K. Juttner and W. J. Lorenz, *Electrochim. Acta*, 28 (1983) 171.
- 6. S. Gudić, J. Radošević and M. Kliškić, J. Appl. Electrochem., 26 (1996) 1027.
- 7. S. Gudić, J. Radošević, D. Krpan-Lisica and M. Kliškić, *Electrochim. Acta*, 46 (2001) 2515.
- 8. S. S. Abdel Rehim, H. H. Hassan and M. A. Amin, J. Appl. Electrochem., 32 (2002) 1257.
- 9. N. M. Yakovleva, L. Anicai, A. N. Yakovlev, L. Dima, E. Y. Khanina and E. A. Chupakhina, *Inorg. Mater.*, 39 (2003) 58.
- 10. M. Metikoš-Huković and R. Babić, J. Appl. Electrochem., 28 (1998) 433.
- 11. H. Gerengi, G. Bereket and M. Kurtay, J. Taiwan. Inst. Chem. Eng., 58 (2016) 509.
- 12. H. Gerengi, P. Slepski, E. Ozgan and M. Kurtay, Mater. Corros., 66 (2015) 233.
- 13. K. S. Ghosh, S. Mukhopadhyay, B. Konar and B. Mishra, Mater. Corros., 64 (2013) 890.
- 14. J. R. Davis, ASM Specialty Handbook, Aluminum and Aluminum Alloys, ASM International, The Materials Information Society, (1998) Ohio, USA.
- 15. P. J. Gregson and H. M. Flower, in: T. Sheppard (Ed.), Proc. Int. Conf. on Aluminum Technology'86, The Institute of Metals, London, United Kingdom, 1986, 423.
- 16. E. J. Lavernia, T. S. Srivatsan and F. A. Mohamed, J. Mater. Sci., 25 (1990) 1137.
- 17. R. E. Ricker and D. J. Duquette in: C. Baker, P. J. Gregson, S. J. Harris and C. J. Peel (Eds), Aluminum Lithium III, Proc. 3rd Int. Conf. on Aluminum Lithium Alloys, The Institute of Metals, London, United Kingdom, 1986, 581.
- 18. H. F. De Jong and J. H. M. Martens, Aluminum, 61(1985) 416.
- 19. G. Seufert, V. Hoyer, H. Wollmer and U. Arndt, Environ. Pollut., 68 (1990) 205.
- 20. Z. Pilić and I. Martinović, Int. J. Mater. Res., 107 (2016) 925.
- 21. P. L. Lane, J. A. Gray, C. J. E. Smith, in: C. Baker, P. J. Gregson, S. J. Harris, C. J. Peel (Eds.), Proc. 3rd Int. Conf. On Aluminum Lithium Alloys, The Institute of Metals, London, United Kingdom, 1986, 273.
- 22. M. J. Dignam, in: J. O'M. Bockris, B. E. Conway, E. Yeager, R. E. White (Eds.), Comprehensive Treatise of Electrochemistry, Vol. 4., Plenum Pub. Corp., (1981) New York, USA.
- 23. E. M. Patrito, R. M. Torresi, E. P. M. Leiva and V. A. Macagno, *J. Electrochem. Soc.*, 137 (1990) 524.
- 24. V. Brunetti and M. Lopez Teijelo, J. Electroanal. Chem., 613 (2008) 16.
- 25. O. E. Linarez Pérez, M. A. Pérez and M. López Teijelo, J. Electroanal. Chem., 632 (2009) 64.
- 26. A. Conde, M. A. Arenas, A. de Frutos and J. de Damborenea, Electrochim. Acta, 53 (2008) 7760.
- 27. A. Conde and J. de Damborenea, *Electrochim. Acta.*, 43 (1998) 849.
- 28. T. P. Moffat and R. H. Latanision, J. Electrochem. Soc., 139 (1992) 1869.
- 29. S. Omanović and M. Metikoš-Huković, Solid State Ionics, 78 (1995) 69.
- 30. C. J. Boxley, J. J Watkins and H. S. White, *Electrochem. Solid-State Lett.*, 6 (10) (2003) B38.
- 31. A. Güntherschulze and H. Betz, Z. Phys., 71 (1931) 106.
- 32. Z. Szklarska Smialowska, Corros. Sci., 41 (1999) 1743.
- 33. A. A. Girginov, A. S. Zahariev and M. S. Machkova, Mater. Chem. Phys., 76 (2002) 274.
- J. R. Macdonald, Impedance spectroscopy, emphasizing solid materials and systems, Wiley, (1987) New York, USA.
- 35. E. M. A. Martini and I. L. Muller, Corros. Sci., 42 (2000) 443.
- 36. U. Rammelt and G. Reinhard, *Electrochim. Acta*, 35 (1990) 1045.
- 37. M. Metikoš-Huković, Z. Pilić, R. Babić and D. Omanović, Acta Biomater., 2 (2006) 693.

38. B. Benfedda, L. Hamadou, N. Benbrahim, A. Kadri, E. Chainet and F. Charlotc, *J. Electrochem. Soc.*, 159 (8) (2012) C372.

© 2017 The Authors. Published by ESG (<u>www.electrochemsci.org</u>). This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution license (http://creativecommons.org/licenses/by/4.0/).